

Torsion in Buildings with Setbacks and Shear Walls

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ABSTRACT

Tall buildings are frequently built with setbacks and shear walls, which introduce structural irregularity in the vertical plane or horizontal plane. Building codes do not recognize that the equivalent static load approach may not be adequate for determining the seismic load distribution in such buildings. The codified static torsional provisions and dynamic analysis are evaluated vis a vis dynamic methods specified in IS:1893-1984 and NBCC 1990 codes. A 6 storey framed building with setbacks, an 8 storey building with setbacks, and an 8 storey frame-shear wall buildings were selected. The Indian code specifies a torsional amplification factor of 1.5 but does not specify accidental eccentricity. The present work clarifies how to account for the accidental eccentricity in the dynamic analysis. It is concluded that the static provisions of the Indian code are adequate for buildings with setbacks. The need to account for accidental eccentricity. NBCC static results are compared with dynamic results within about 20%.

INTRODUCTION

Most building codes give simplified torsional provisions for regular buildings. Tall buildings only. Such buildings can be analyzed statically using 2-D modelling. For buildings with setbacks and shear walls, a 3-D dynamic analysis is recommended by almost all codes. The applicability of the static torsional provisions of IS:1893-1984 and NBCC 1990 for buildings with setbacks and shear walls. The analyses were performed using both the static approach as well as the response spectrum approach. Recently, Jain and Annigeri studied the static and dynamic provisions of the NBCC 1990 for buildings with setbacks and observed that the static base shear is within 20% of the dynamic base shear. They concluded that the equivalent static method can be used for the design of such buildings. The present work is extended to shear wall buildings.

METHOD OF ANALYSIS

The Indian code and the Canadian code require the calculation of the design eccentricity for the static analysis of asymmetrical buildings. The design eccentricity is given by

$$e_a = \alpha e + \beta D_n \quad \text{and} \quad e_b = \gamma e - \beta D_n$$

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setback building (Fig. 4b) as well as its frame 1 and frame 2 by 10% (Fig. 6).

The total shears in each frame of the 8 storey setback building obtained by the NBCC methods are shown in Fig. 7. It can be seen that the NBCC static method underestimates the base shear in the edge frame 1 by up to 18%. It gives conservative results elsewhere in this setback building. A similar observation was made by Tso and Yao (1994) in their 8 storey setback building. They studied in detail the contribution of different modes on the dynamic response. IS:1893 static method again overestimates the shears by about 20% (not shown). The main difference between the Indian and NBCC specifications is the absence of accidental eccentricity in the former which affects the dynamic response significantly.

Twelve storey buildings

The static and dynamic frame shears in the 12 storey frame building and the shear wall building are shown in Figs. 8, 9 and 10. The dynamic base shears were magnified so that they were equal to those given by the static base shear before carrying out the torsional analysis. The 12 storey frame building was asymmetric but without any irregularity in the vertical plane as defined in the Indian or Canadian codes. In the frame building, therefore, both the codified static and dynamic methods are applicable. IS:1893 static method again overestimates the shears by about 20% (not shown). It can be seen that the NBCC static frame shear is less in frame 2 in the upper four storeys and in the entire frame 3 by about 10% than the corresponding dynamic values (Fig. 8).

The static and dynamic frame shears in the shear wall building are shown in Figs. 9 and 10 in accordance with the IS:1893 and NBCC respectively. The NBCC static provisions overestimate the total storey shears in this building by 30% (not shown). The frame shears are overestimated except in the upper storeys of the flexible edge frame 3 (Fig. 10).

UBC dynamic method vs. NEHRP dynamic method

The results of these two dynamic methods were also shown in Figs. 6 to 10. It can be easily seen that the frame shears in the building are within 10% of each other in all cases. The difference in the frame shears is generally about 25% and the trend is mixed. In terms of the efforts, there is not much difference in the two methods. Both require a set of three analyses. The UBC dynamic method requires three dynamic analyses and the envelope is obtained, while the NEHRP method requires one dynamic analysis and two static analyses and then the results are added so as to get the worst effect. The UBC dynamic approach is preferred.

CONCLUSIONS

Based on the results presented in this research work, the following significant conclusions can be derived :

- (1) IS:1893 static approach gives very conservative results as compared with the IS dynamic approach in all the buildings considered in this paper. This is because of the presence of a large dynamic magnification factor of 1.5 in the static design eccentricity and the absence of the accidental factor in the dynamic analysis.
- (2) The NBCC static provisions underestimate the base shear and frame shears in the setback building by upto 18%, and in the 12 storey frame building by upto 10% as compared with those of the NEHRP dynamic method. In the shear wall building, the NBCC static provisions overestimate the frame shears by upto 30%.
- (3) The static methods do not account for higher modes. They may be used for preliminary design of such irregular buildings. However, for the final design, dynamic analysis must

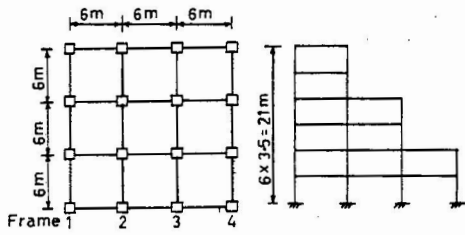


Fig. 1. 6 storey frame building with setbacks

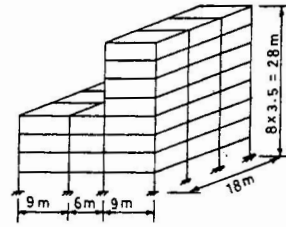


Fig. 2. 8 storey frame building with setback

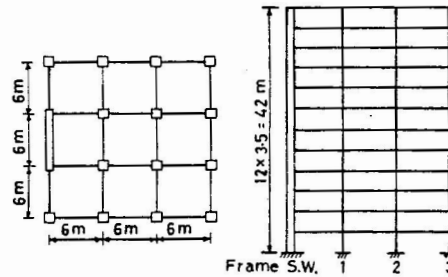


Fig. 3. 12 storey frame-shear wall building

6 storey frame building with setbacks

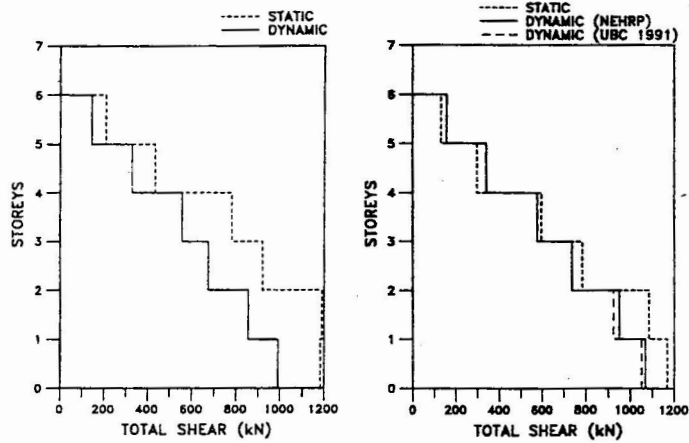


Fig. 4. Comparison of total storey shears in 6 storey frame building with setbacks, based on code torsional provisions (a) IS:1893 (b) NBCC 1990

